Energetic Galerkin Projection of Electromagnetic Fields between Different Meshes

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*Abstract***—In order to project electromagnetic fields between di**ff**erent meshes with respect to the conservation of energetic values, Galerkin projection formulations based on the energetic norm are developed in this communication. The proposed formulations are applied to an academic example.**

*Index Terms***—Finite element methods, Galerkin method, Interpolation, Modeling, Projection.**

I. Introduction

In recent years, the numerical studies of coupled problems are more and more investigated. These studies deal with the interactions between different physical phenomena, e.g. electromagnetic - thermal or magnetic - mechanic. According to the importance of the interaction, coupled problems can be treated with different strategies. One possibility is that the study domain is discretized on different meshes for different problems. In this case, it is necessary to communicate and transfer fields between different meshes. In the literature, the concept of Galerkin projection based on the L^2 error norm provides a very convenient tool to carry out this transfer [**?**], [**?**], [**?**]. In comparison to the direct interpolation, Galerkin projection enjoys several advantages, especially in terms of precision. However, using this method, the conservation of the energy is not assured between the original and target meshes [**?**]. To tackle this issue, formulations deduced from the minimization of the energetic norm can be used.

In this communication, energetic approaches for Galerkin projection are developed in order to conserve the magnetic energy and electric power between different meshes. Firstly, the numerical models developed from the minimization of the energetic norm are presented for magneto-static and eddy current problems. Secondly, the obtained formulations are applied to an academic example.

II. Energetic Galerkin projection formulations

Given a solution of electromagnetic computation on a source mesh, we aim to project this result onto a target mesh which differs. The energetic Galerkin projection formulations are investigated for magneto-static problems as well as eddy current problems.

A. Magneto-static problems

In order to solve magneto-static problems, different formulations such as the formulations based on scalar or vectorial potentials can be employed. As a result, either the magnetic

field **H** or the magnetic flux density **B** is conformed with physical properties. We denote by H_s and B_s the fields obtained on the source mesh and by H_t and B_t the fields to be calculated on the target mesh. The energetic norms of the interpolation error are defined as:

$$
\varepsilon_{\mathbf{H}} = \int_{D} \mu \left| \mathbf{H}_{t} - \mathbf{H}_{s} \right|^{2} d\tau \tag{1}
$$

$$
\varepsilon_{\mathbf{B}} = \int_{D} \frac{1}{\mu} \left| \mathbf{B}_{t} - \mathbf{B}_{s} \right|^{2} d\tau \tag{2}
$$

with μ the linear magnetic permeability.

Using Whitney elements in 3D, H_t and B_t are discretized in the edge and facet element spaces respectively such that $\mathbf{H}_t = \sum \mathbf{w}_i^e h_i$ and $\mathbf{B}_t = \sum \mathbf{w}_i^f$ $\int_i^f b_i$. Here \mathbf{w}_i^e (resp. \mathbf{w}_i^f) $\binom{J}{i}$ and h_i (resp. $\overline{b_i}$) are the shape functions and the values of H_t (resp. **B***t*) associated with the *i*−*th* edge (resp. facet). To project fields onto a target mesh with respect to the magnetic energy, weak formulations based on the minimization of the energetic norm are developed. In (1), the energetic error norm is minimized when its derivatives with respect to all degrees of freedom are equal to zero, thus for each edge *i*:

$$
\frac{\partial}{\partial h_i} \int_D \mu |\mathbf{H}_t - \mathbf{H}_s|^2 d\tau = 0
$$
 (3)

$$
\int_{D} \mu(\mathbf{w}_{i}^{e} \cdot \mathbf{H}_{t} - \mathbf{w}_{i}^{e} \cdot \mathbf{H}_{s}) d\tau = 0
$$
\n(4)

Finally, the matrix equation to solve can be written:

$$
[C][h] = [F] \tag{5}
$$

where $C_{ij} =$ *D* $\mu \mathbf{w}_i^e \cdot \mathbf{w}_j^e d\tau, F_i =$ *D* $\mu \mathbf{w}_i^e \cdot \mathbf{H}_s d\tau$ and $[h]$ is the vector of degrees of freedom to be calculated.

A similar demonstration can be applied to (2) for the projection of **B***^s* with respect to the magnetic energy.

B. Eddy current problems

For eddy current problems, either magnetic or electric harmonic formulations can be used in order to calculate harmonic fields. We obtain either H_s or E_s conformed with physical properties. Thus, depending on the used formulation, the energetic error norm to minimize can be defined [**?**]:

$$
\varepsilon_{\mathbf{H}} = \int_{D} \mu \left| \mathbf{H}_{t} - \mathbf{H}_{s} \right|^{2} d\tau + \int_{D_{c}} \frac{1}{\sigma \omega} \left| \mathbf{curl} \mathbf{H}_{t} - \mathbf{curl} \mathbf{H}_{s} \right|^{2} d\tau \tag{6}
$$

$$
\varepsilon_{\mathbf{E}} = \int_{D_c} \frac{\sigma}{\omega} \left| \mathbf{E}_t - \mathbf{E}_s \right|^2 d\tau + \int_{D} \frac{1}{\mu} \left| \frac{\text{curl } \mathbf{E}_t - \text{curl } \mathbf{E}_s}{\omega} \right|^2 d\tau \tag{7}
$$

with σ the electrical conductivity and ω the pulsation.

In order to project fields onto a target mesh with respect to the magnetic energy in *D* and electric power in conducting domain *Dc*, weak formulations can be obtained by the minimization of the energetic norm. Equation (6) gives rise to matrix equation:

$$
([C] + [C_e]) [h] = [F] + [F_e]
$$
 (8)

where [*C*] and [*F*] are the same matrix as in magneto-static problems, $C_{eij} = \int \frac{1}{\sqrt{2\pi}}$ \int ^{D_c</sub> \int ^D_c</sub>} $\frac{1}{\sigma \omega}$ **curl w**^{*e*}_{*i*}*d***r** and F_{ei} = *Dc* 1 $\frac{1}{\sigma\omega}$ curl **w**^{*e*} · curl **H**_{*s}d* τ . Here $[C] + [C_e]$ is a positive-</sub> definite matrix.

A similar matrix system can be obtained from (7) in order to project **E***^s* .

III. Application

The proposed projection formulations are applied in an academic example. This example is composed of a magnetic core cylinder and an excitation coil (Fig. 1). Two meshes are considered: Ms (306K elements) and Mt (60K elements). In order to carry out projections, Ms is used as the source mesh for the first computation and Mt is considered as the target mesh for the projection.

Firstly, a constant current is applied in the coil. The magneto-static problem is solved on Ms or Mt using the scalar potential formulation. The obtained field H_s on Ms is then projected to Mt using (5). The corresponding magnetic flux density on the clipping plane (S in Fig. 1) is presented in Fig. 2a. In order to illustrate the advantage of the projection method, the field \mathbf{H}_s is also projected using a classical L^2 norm projection (Fig. 2b). In comparison to the energetic projection, the L^2 projection fails to provide a correct distribution of **B** at the boundary of the cylinder. Table I presents the max values of fields and the magnetic energy calculated on Ms and Mt alone for reference, and then from Ms to Mt projections. With the formulation deduced from the minimization of the energetic norm, the magnetic energy and the max values of fields are close to the reference results (calculated on Mt alone).

Secondly, a sinusoidal current is applied as excitation. In this case, eddy currents appear in the conductor cylinder. The magneto harmonic problem is solved with the magnetic formulation. Table II presents the reference results (calculated on Ms and Mt alone) for the max values of fields, the magnetic energy in the domain and the ohmic losses in the cylinder. As the L^2 projection fails to conserve the magnetic energy and the ohmic losses, only the results obtained using the energetic projection are shown. They are obtained using (8). In this example, the magnetic energy as well as the ohmic losses are well conserved using the energetic Galerkin projection.

Figure 1: Geometry of the example

Figure 2: Distribution of **B** (T) on a clipping plane, calculated from the projected H_t field.

Table I: Validation of the energetic projection approach (magneto-static problem)

	magnetic energy	$\left \mathbf{H} \right _{max}$	\mathbf{B} _{max}
	(mJ)	(kA/m)	(T)
calculated on Ms	8.01	44.1	0.116
calculated on Mt.	8.25	49.0	0.096
L^2 proj. Ms \rightarrow Mt	10.28	42.9	4.17
energetic proj. Ms→Mt	7.32	45.3	0.089

Table II: Validation of the energetic projection approach (eddy current problem)

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